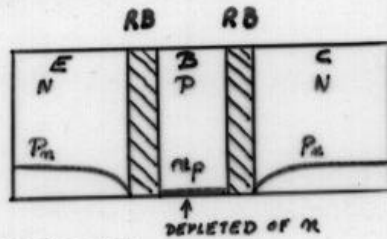
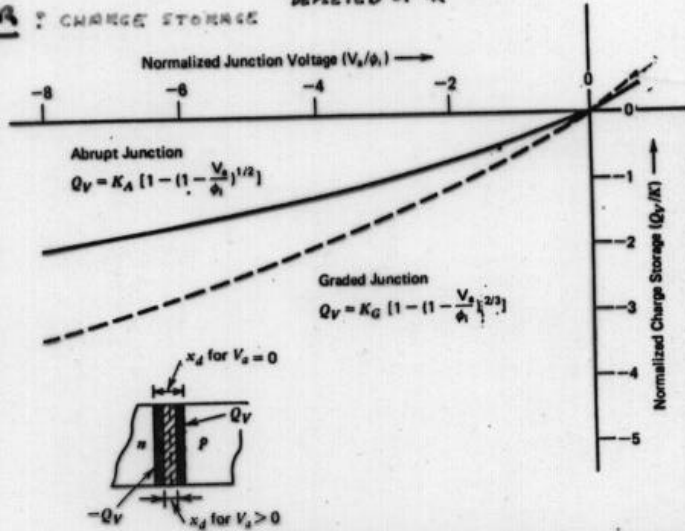


TRANSISTOR SWITCHING : STORAGE, EXTRACTION AND TRANSPORT OF \bar{e} IN THE BASE

CUT-OFF



CAPACITOR : CHARGE STORAGE

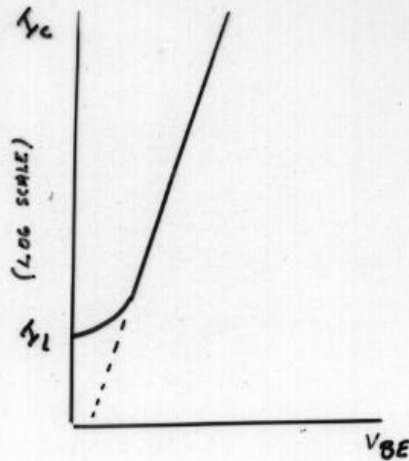


$$K_A = (2 \epsilon_s q N_A \phi_j)^{1/2}$$

$$K_G = \frac{1}{8} (12 \epsilon_s \phi_j (q a)^2)^{1/3}$$

Figure 6.8 Normalized stored charge Q_V/K versus normalized junction bias V_j/ϕ_j in the space-charge regions of an abrupt junction and a linearly graded junction.

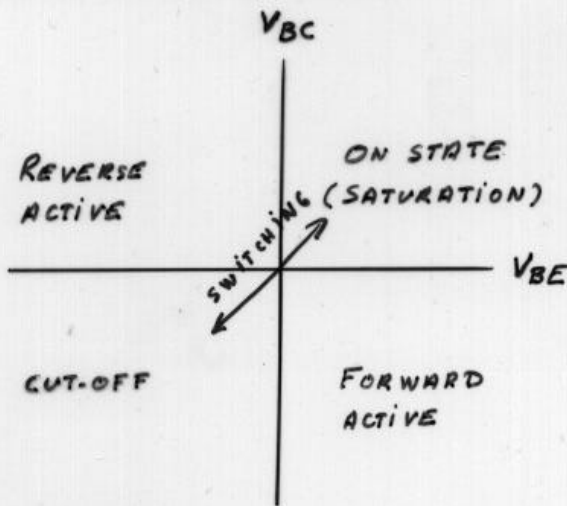
CUT OFF IS NOT AN OPEN-CIRCUIT



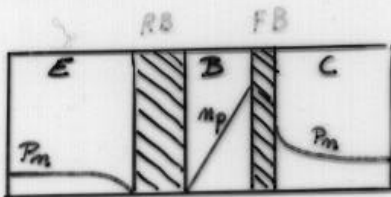
I_{c2} : GENERATION OF HOLES AND ELECTRONS IN COLLECTOR JUNCTION SPACE CHARGE REGION

$$I_{c2} = J_c A_c = I_{g2} = \frac{1}{2} q n_i x_d A_c / \tau_0$$

REGIONS OF OPERATION



REVERSE ACTIVE: PARAMETERS: $F \rightarrow R$ $\beta_R = \left| \frac{I_E}{I_B} \right|$



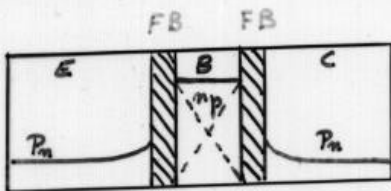
IN PROTOTYPE TRANSISTORS: SYMMETRIC. $RA = FA$

IN β_C TRANSISTORS: RA IS DIFFERENT FROM FA

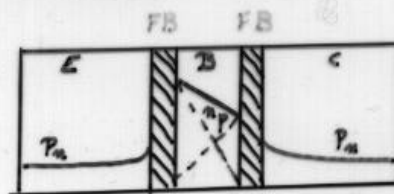
RA PERFORMANCES \ll FA PERFORMANCES

$$\beta_R < \beta_F$$

SATURATION: EACH JUNCTION INJECTS AND COLLECTS CARRIERS



NO CURRENT BETWEEN E AND C



CURRENT FLOWING FROM E TO C.

EBERS-MOLL MODEL (1954)

LINKING CURRENT:
$$I_m = I_s \left(e^{\frac{qV_{BC}}{KT}} - e^{\frac{qV_{BE}}{KT}} \right)$$

DOES NOT ACCOUNT FOR THE COMPONENTS OF BASE CURRENTS: $\underline{I_{BE}}$ AND $\underline{I_{BC}}$.



$$\begin{cases} I_E = I_m - I_{BE} \\ I_C = -I_m - I_{BC} \end{cases}$$

$$\begin{cases} I_m = I_s \left(e^{\frac{qV_{BC}}{KT}} - e^{\frac{qV_{BE}}{KT}} \right) & I_s = I_s A \\ I_{BE} = I_{0E} \left(e^{\frac{qV_{BE}}{KT}} - 1 \right) & \text{- EMITTER JUNCTION} \\ I_{BC} = I_{0C} \left(e^{\frac{qV_{BC}}{KT}} - 1 \right) & \text{- COLLECTOR JUNCTION} \end{cases}$$

$$\begin{aligned} I_E &= -(I_s + I_{0E}) \left(e^{\frac{qV_{BE}}{KT}} - 1 \right) + I_s \left(e^{\frac{qV_{BC}}{KT}} - 1 \right) \\ I_C &= -(I_s + I_{0C}) \left(e^{\frac{qV_{BC}}{KT}} - 1 \right) + I_s \left(e^{\frac{qV_{BE}}{KT}} - 1 \right) \end{aligned}$$

WITH

$$\begin{cases} I_{ES} = I_s + I_{0E} & I_{CS} = I_s + I_{0C} \\ \alpha_F = \frac{I_s}{I_{ES}} & \alpha_R = \frac{I_s}{I_{CS}} \end{cases}$$

$$\begin{cases} I_E = -I_{ES} \left(e^{\frac{qV_{BE}}{KT}} - 1 \right) + \alpha_R I_{CS} \left(e^{\frac{qV_{BC}}{KT}} - 1 \right) \\ I_C = -I_{CS} \left(e^{\frac{qV_{BC}}{KT}} - 1 \right) + \alpha_F I_{ES} \left(e^{\frac{qV_{BE}}{KT}} - 1 \right) \end{cases}$$

EBERS-MOLL EQUATIONS

4 PARAMETERS: $I_{ES}, I_{CS}, \alpha_R, \alpha_F$

KIRCHOFF'S LAW
$$I_E + I_B + I_C = 0$$

RECIPROCALITY RELATION
$$\alpha_R I_{CS} = \alpha_F I_{ES} = I_s$$

TWO ADDITIONAL RELATIONS.

EBERS-MOLL EQUATION

$$I_E = -I_{ES} \left(e^{\frac{qV_{BE}}{kT}} - 1 \right) + \alpha_R I_{CS} \left(e^{\frac{qV_{BC}}{kT}} - 1 \right)$$

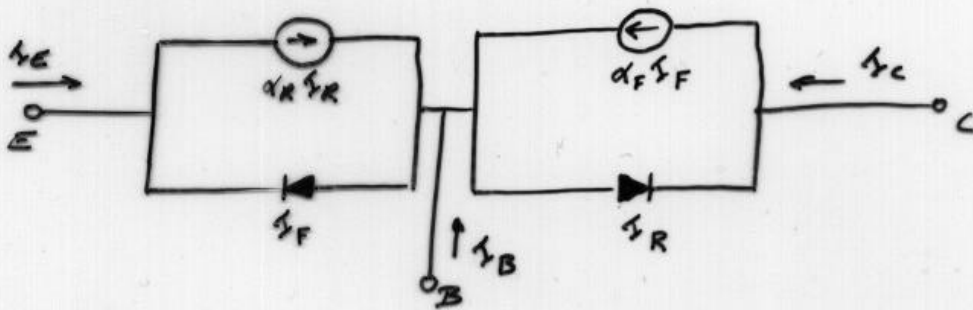
$$I_C = -I_{CS} \left(e^{\frac{qV_{BC}}{kT}} - 1 \right) + \alpha_F I_{ES} \left(e^{\frac{qV_{BE}}{kT}} - 1 \right)$$

OR

$$\begin{cases} I_E = -I_F + \alpha_R I_R \\ I_C = -I_R + \alpha_F I_F \end{cases}$$

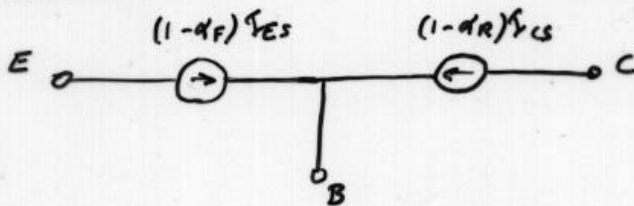
$$\begin{cases} I_F = I_{ES} \left(e^{\frac{qV_{BE}}{kT}} - 1 \right) \\ I_R = I_{CS} \left(e^{\frac{qV_{BC}}{kT}} - 1 \right) \end{cases}$$

EQUIVALENT CIRCUIT



$$I_B = -(I_E + I_C) = I_F(1 - \alpha_F) + I_R(1 - \alpha_R)$$

APPLICATION: CUTOFF $V_{BE} < 0, V_{BC} < 0$



APPLICATIONS

$$\begin{cases} I_E = -I_F + \alpha_R I_R & (1) \\ I_C = -I_R + \alpha_F I_F & (2) \end{cases}$$

IN FORWARD ACTIVE MODE

α_F (1) AND REPLACE IN (2)

$$I_C = -\alpha_F I_E - I_R (1 - \alpha_F \alpha_R)$$

$$I_C = -\alpha_F I_E + I_{CS} (1 - \alpha_F \alpha_R)$$

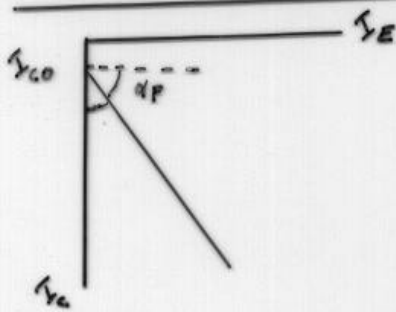
SINCE COLLECTOR IS REVERSE BIASED

IN REVERSE ACTIVE MODE

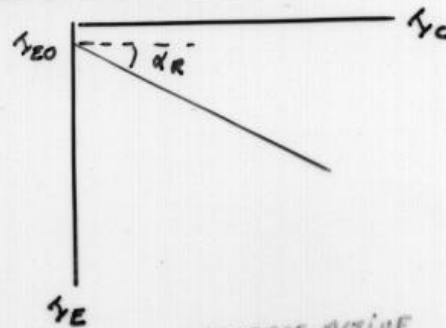
$$I_E = -\alpha_R I_C + I_{ES} (1 - \alpha_F \alpha_R)$$

SIMILARLY SINCE EMITTER IS REVERSE BIASED

EXPERIMENTAL DETERMINATION OF α_F , α_R , I_{ES} AND I_{CS}



FORWARD-ACTIVE



REVERSE-ACTIVE

OPEN CIRCUITED EMITTER

$$I_{CO} = I_C |_{I_E=0} = I_{CS} (1 - \alpha_F \alpha_R)$$

OPEN CIRCUITED COLLECTOR

$$I_{EO} = I_E |_{I_C=0} = I_{ES} (1 - \alpha_F \alpha_R)$$

COMPARISON WITH $I_{CEO} = I_E |_{I_B=0}$

$$I_B = -(I_C + I_E) = 0 \Rightarrow I_E = -I_C$$

$$I_C = +\alpha_F I_C + I_{CS} (1 - \alpha_F \alpha_R)$$

$$I_{CEO} = \frac{I_{CS} (1 - \alpha_F \alpha_R)}{1 - \alpha_F}$$

AMPLIFICATION OF I_{CO}

$$I_{CEO} = \frac{I_{CO}}{1 - \alpha_F}$$

