

Digital Modulation

- After possible source and error control encoding, we have a sequence $\{m_n\}$ of message symbols to be transmitted on the channel. The message symbols are assumed to come from a finite alphabet, say $\{0, 1, \dots, M-1\}$. In the simplest case of binary signaling, $M = 2$. Each symbol in the sequence is assigned to one of M waveforms $\{s_0(t), \dots, s_{M-1}(t)\}$.
- *Memoryless modulation versus modulation with memory.* If the symbol to waveform mapping is fixed from one interval to the next, i.e., $m \mapsto s_m(t)$, then the modulation is memoryless. If the mapping from symbol to waveform in the n -th symbol interval depends on previously transmitted symbols (or waveforms) then the modulation is said to have memory.
- For memoryless modulation, to send the sequence $\{m_n\}$ of symbols at the rate of $1/T_s$ symbols per second, we transmit the signal

$$s(t) = \sum_n s_{m_n}(t - nT_s). \quad (1)$$

- *Linear versus nonlinear modulation.* A digital modulation scheme is said to be linear if we can write the mapping from the sequence of symbols $\{m_n\}$ to the transmitted signal $s(t)$ as concatenation of a mapping from the sequence $\{m_n\}$ to a complex sequence $\{c_n\}$, followed by a *linear* mapping from $\{c_n\}$ to $s(t)$. Otherwise the modulation is nonlinear.

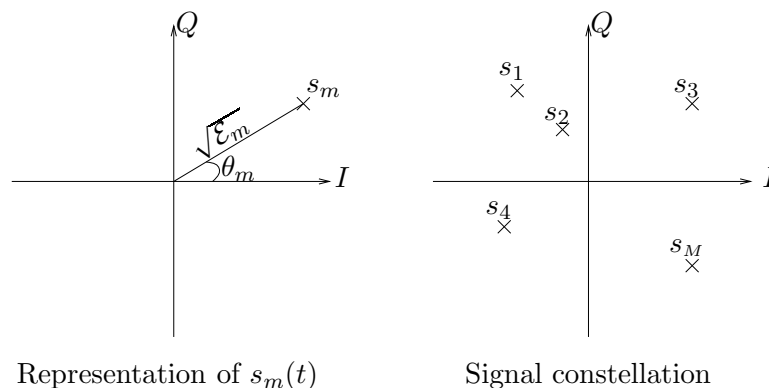
Linear Memoryless Modulation

- In this case, the mapping from symbols to waveforms can be written in complex baseband as:

$$s_m(t) = \sqrt{\mathcal{E}_m} e^{j\theta_m} g(t), \quad m = 1, 2, \dots, M, \quad (2)$$

where $g(t)$ is a real-valued, unit energy, pulse shaping waveform.

- The signal $s_m(t)$ can be represented by a point in the complex plane, i.e., the signal space corresponding to a symbol interval is a 1-d (complex) space with basis function $g(t)$.



- In real passband,

$$\tilde{s}_m(t) = \text{Re}[\sqrt{2}s_m(t)e^{j2\pi f_c t}] = \sqrt{2\mathcal{E}_m} \cos(2\pi f_c t + \theta_m)g(t). \quad (3)$$

- As we saw in class, the signal energy is the same in both the real passband and complex baseband domains and equals \mathcal{E}_m .
- The average symbol energy for the constellation is given by

$$\mathcal{E}_s = \frac{1}{M} \sum_{m=1}^M \mathcal{E}_m. \quad (4)$$

- The average bit energy for the constellation (assuming that $M = 2^\nu$, for some integer ν) is given by

$$\mathcal{E}_b = \frac{\mathcal{E}_s}{\log_2 M} = \frac{\mathcal{E}_s}{\nu}. \quad (5)$$

- The distance between signals s_k and s_m is $d_{k,m} = \|s_k - s_m\|$, and the minimum distance is given by

$$d_{\min} = \min_{k,m} d_{k,m}. \quad (6)$$

- A measure of goodness of the constellation is the ratio

$$\zeta = \frac{d_{\min}^2}{\mathcal{E}_b}. \quad (7)$$

Note that ζ is independent of scaling of the constellation.

- Some commonly used signal constellations are:

- *Pulse Amplitude Modulation (PAM)*. Information only in amplitude:

$$\theta_m = 0 \text{ and } \sqrt{\mathcal{E}_m} = (2m - 1 - M)\frac{d}{2}, \quad m = 1, 2, \dots, M. \quad (8)$$

We can compute ζ as a function of M . For example, $\zeta = 4$ for $M = 2$.

- *Phase Modulation or Phase Shift Keying (PSK)*. Information only in phase:

$$\theta_m = \frac{2\pi m}{M} \text{ and } \mathcal{E}_m = \mathcal{E}, \quad m = 1, 2, \dots, M. \quad (9)$$

We showed in class that

$$d_{\min} = \sqrt{2\mathcal{E} \left(1 - \cos \frac{2\pi}{M}\right)} \implies \zeta = 2 \log_2 M \left(1 - \cos \frac{2\pi}{M}\right)$$

For QPSK, $\zeta = 4$ (as in BPSK).

- *Quadrature Amplitude Modulation (QAM)*. Information in phase and amplitude. We can design constellations to maximize ζ for a given M . Rectangular constellations are convenient for demodulation. For rectangular 16-QAM, $\zeta = 1.6$.

Orthogonal Memoryless Modulation

- Here the signal set is given by

$$s_m(t) = \sqrt{\mathcal{E}} g_m(t), \quad m = 1, 2, \dots, M \quad (10)$$

where $\{g_m(t)\}$ are (possibly complex) unit energy signals, i.e., $\|g_m(t)\| = 1$.

- The correlation between signals $s_k(t)$ and $s_m(t)$ is given by:

$$\rho_{km} = \frac{\langle s_k(t), s_m(t) \rangle}{\mathcal{E}} = \langle g_k(t), g_m(t) \rangle \quad (11)$$

- There are two kinds of orthogonality:

- Orthogonality only in the real component of the correlation, i.e. $\text{Re}\{\rho_{km}\} = 0$, for $k \neq m$. This form of orthogonality is enough for coherent demodulation.
- Complete orthogonality, i.e., $\rho_{km} = 0$, for $k \neq m$. This is required for noncoherent demodulation.

- *Examples of orthogonal signal sets*

- *Separation in time:*

$$g_m(t) = g(t - (m-1)T_s/M) \quad (12)$$

where $g(t)$ is such that $\langle g(t - kT_s/M), g(t - mT_s/M) \rangle = \delta_{km}$. For example, $g(t) = p_{T_s/M}(t)$, a rectangular pulse of width T_s/M .

This signal set is completely orthogonal. We can also create a signal set of twice the size which satisfies orthogonality only in the real component of the correlation by adding $\{jg_m(t)\}$ to the above signal set as we saw in class.

- *Separation in frequency:*

$$g_m(t) = e^{j2\pi(m-1)\Delta_f t} p_{T_s}(t) \quad (13)$$

It is easy to show that

$$\rho_{km} = \text{sinc}[T_s(k-m)\Delta_f] e^{j\pi T_s(k-m)\Delta_f} \quad (14)$$

and that

$$\text{Re}\{\rho_{km}\} = \text{sinc}[2T_s(k-m)\Delta_f]. \quad (15)$$

Thus the smallest value of Δ_f such that $\rho_{km} = 0$, for $k \neq m$, is $1/T_s$, and such that $\text{Re}\{\rho_{km}\} = 0$, for $k \neq m$, is $1/2T_s$.

- *Separation in time and frequency:* One way to do this is to pick $\{g_m(t)\}$ to be the Walsh-Hadamard functions on $[0, T_s]$ as we saw in class.