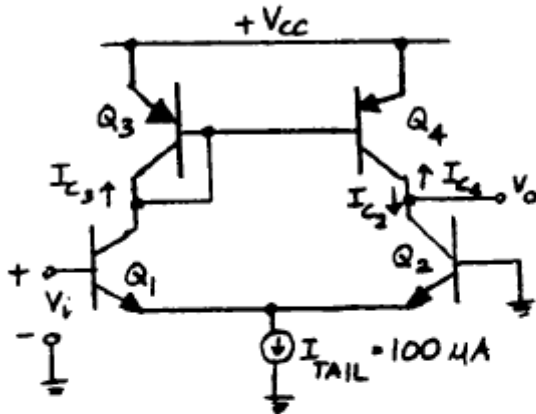


4.12

$$V_{A_{\text{PNP}}} = 50 \text{ V} \quad V_{A_{\text{NPN}}} = 130 \text{ V}$$

$$\beta_{F_{\text{PNP}}} = 50 \quad \beta_{F_{\text{NPN}}} = 200$$

Assume no device mismatch



$$I_{C1} \approx I_{C2} = \frac{I_{EE}}{2} = 50 \mu\text{A} = I_C$$

$$I_{C3} \approx I_{C4} = -50 \mu\text{A}$$

$$\therefore g_m = \frac{I_C}{V_T} = \frac{50 \mu\text{A}}{26 \text{ mV}} = \frac{1}{520} \text{ V}^{-1}$$

$$r_{o_{\text{PNP}}} = \frac{V_{A_{\text{PNP}}}}{I_C} = 1 \text{ M}\Omega$$

$$r_{o_{\text{NPN}}} = \frac{V_{A_{\text{NPN}}}}{I_C} = 2.6 \text{ M}\Omega$$

since unloaded, the output resistance is

$$R_{\text{OUT}} = r_{o_{\text{PNP}}} \parallel r_{o_{\text{NPN}}} = 722 \text{ k}\Omega$$

$$A_V = g_m R_{\text{OUT}} = \frac{1}{520} \times 722 \text{ k} \\ = 1388$$

BJT DIFFERENTIAL PAIR WITH CURRENT-MIRROR LOAD

VCC 100 0 2.5
VBE 200 0 -2.5
Q1 2 3 4 NPN
Q2 6 0 4 NPN
Q3 2 2 100 PNP
Q4 6 2 100 PNP
ITAIL 4 200 100U
RTAIL 4 200 1MEG
.MODEL NPN NPN RB=200 BF=200 VAF=130 IS=5E-15
.MODEL PNP PNP RB=300 BF=50 VAF=50 IS=2E-15

* A DC INPUT VOLTAGE OF ABOUT 1 MV FORCES THE COLLECTOR-EMITTER
* VOLTAGE OF Q2 ABOUT EQUAL TO THAT OF Q1.

VDC 3 5 1M
VI 5 0
.OPTIONS NOMOD NOPAGE
.WIDTH OUT=80
.OP
.DC VI -0.01 0.01 0.002
.PLOT DC V(6)
.TF V(6) VI
.END

***** DC TRANSFER CURVES TNOH= 27.000 TEMP= 27.000

Table with columns: VOLT, V(6), and data points for current and voltage at various bias points.

**** OPERATING POINT INFORMATION TNOH= 27.000 TEMP= 27.000
NODE =VOLTAGE NODE =VOLTAGE NODE =VOLTAGE
+0:2 = 1.880E+00 0:3 = 1.000E-03 0:4 = -5.951E-01
+0:5 = 0. 0:6 = 1.857E+00 0:100 = 2.500E+00
+0:200 = -2.500E+00

**** BIPOLAR JUNCTION TRANSISTORS

Table with columns: SUBCJT, ELEMENT, MODEL, IB, IC, VBE, VCE, VBC, VS, POWER, BETA, GM, RPI, RX, RO, BETAAC and corresponding values for nodes 0:Q1, 0:Q2, 0:Q3, 0:Q4.

**** SMALL-SIGNAL TRANSFER CHARACTERISTICS

V(6)/VI = 1.398E+03
INPUT RESISTANCE AT VI = 2.853E+05
OUTPUT RESISTANCE AT V(6) = 7.294E+05

BJT DIFFERENTIAL PAIR WITH CURRENT-MIRROR LOAD

* (COMMON-MODE INPUT)
VCC 100 0 2.5
VBE 200 0 -2.5
Q1 2 3 4 NPN
Q2 6 5 4 NPN
* [CMRR] = 1398/0.0002561 = 5.462E
Q3 2 2 100 PNP
Q4 6 2 100 PNP
ITAIL 4 200 100U
RTAIL 4 200 1MEG
.MODEL NPN NPN RB=200 BF=200 VAF=130 IS=5E-15
.MODEL PNP PNP RB=300 BF=50 VAF=50 IS=2E-15

* A DC INPUT VOLTAGE OF ABOUT 1 MV FORCES THE COLLECTOR-EMITTER
* VOLTAGE OF Q2 ABOUT EQUAL TO THAT OF Q1.

VDC 3 5 1M
VI 5 0
.OPTIONS NOMOD NOPAGE
.WIDTH OUT=80
.OP
.DC VI -0.01 0.01 0.002
.PLOT DC V(6)
.TF V(6) VI
.END

***** DC TRANSFER CURVES TNOH= 27.000 TEMP= 27.000

Table with columns: VOLT, V(6), and data points for current and voltage at various bias points.

**** OPERATING POINT INFORMATION TNOH= 27.000 TEMP= 27.000
NODE =VOLTAGE NODE =VOLTAGE NODE =VOLTAGE
+0:2 = 1.880E+00 0:3 = 1.000E-03 0:4 = -5.951E-01
+0:5 = 0. 0:6 = 1.857E+00 0:100 = 2.500E+00
+0:200 = -2.500E+00

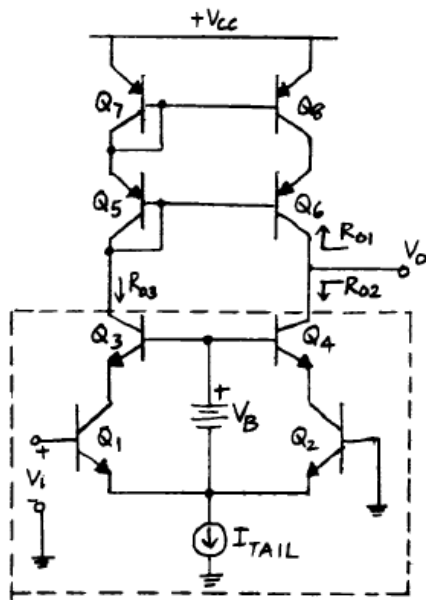
**** BIPOLAR JUNCTION TRANSISTORS

Table with columns: SUBCJT, ELEMENT, MODEL, IB, IC, VBE, VCE, VBC, VS, POWER, BETA, GM, RPI, RX, RO, BETAAC and corresponding values for nodes 0:Q1, 0:Q2, 0:Q3, 0:Q4.

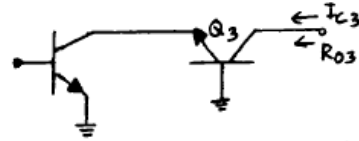
**** SMALL-SIGNAL TRANSFER CHARACTERISTICS

V(6)/VI = -2.561E-04
INPUT RESISTANCE AT VI = 1.152E+08
OUTPUT RESISTANCE AT V(6) = 7.294E+05

4.16

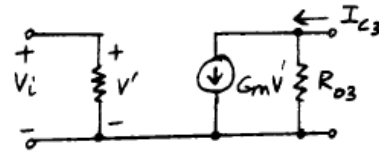


Half circuit of the dotted box :



is the CE-CB configuration.

∴ the equivalent circuit is



Where $R_i = r_{\pi 1}$, $G_m = g_{m1}$

$$R_{O3} = \beta_3 r_{O3} = \beta_4 r_{O4} = R_{O2}$$

$$R_{OUT} = R_{O1} \parallel R_{O2}$$

$$R_{O1} \approx \frac{\beta_c r_{O6}}{2}$$

$$I_{C1} = I_{C2} = I_{C3} = I_{C4} = -I_{C5} = -I_{C6} \\ = -I_{C7} = -I_{C8} = I_{EE}/2$$

$$\therefore g_{m1} = g_{m2} = g_{m3} = g_{m4} = g_{m5} \\ = g_{m6} = g_{m7} = g_{m8} = g_m$$

$$\beta_4 = \beta_{npn} = 200, \beta_c = \beta_{pnp} = 50$$

$$\therefore r_{O6} = \frac{1}{g_m \eta_{pnp}}, r_{O4} = \frac{1}{g_m \eta_{npn}}$$

$$R_{OUT} = R_{O1} \parallel R_{O2}$$

$$= \frac{1}{\frac{2g_m \eta_{pnp}}{\beta_c} + \frac{g_m \eta_{npn}}{\beta_4}}$$

$$A_V = g_m R_{OUT} = \frac{1}{\frac{2\eta_{pnp}}{\beta_c} + \frac{\eta_{npn}}{\beta_4}}$$

$$A_V = \left[\frac{1}{\left(\frac{2 \times 5 \times 10^{-4}}{50} + \frac{2 \times 10^{-4}}{200} \right)} \right] = 4.8 \times 10^4$$

BJT CASCODED DIFFERENTIAL PAIR WITH CASCODED CURRENT-MIRROR LOAD

```
VCC 100 0 2.5
VEE 200 0 -2.5
VBIAS 9 2 1.3
Q1 3 1 2 NPN
Q2 4 0 2 NPN
Q3 5 9 3 NPN
Q4 6 9 4 NPN
Q5 5 5 7 PNP
Q6 6 5 8 PNP
Q7 7 7 100 PNP
Q8 8 7 100 PNP
ITAIL 2 200 100U
RTAIL 2 200 1MEG
.MODEL NPN NPN RB=200 BF=200 VAF=130 IS=5E-15
.MODEL PNP PNP RB=300 BF=50 VAF=50 IS=2E-15
```

- * A DC INPUT VOLTAGE OF ABOUT 2 MV FORCES THE VOLTAGE FROM
- * THE OUTPUT TO GROUND TO BE ABOUT EQUAL TO THE VOLTAGE
- * FROM NODE 5 (THE CASCODE CURRENT MIRROR INPUT) TO GROUND.

```
VIDC 1 10 2M
VI 10 0
.OPTIONS NOMOD NOPAGE
.WIDTH OUT=80
.OP
.DC VIDC -0.01 0.01 0.001
.PLOT DC V(6)
.TF V(6) VI
.END
```

******* DC TRANSFER CURVES TNOH= 27.000 TEMP= 27.000**

IA	VOLT	V(6)	5.000E-01	1.000E-00	1.500E+00	2.000E+00
-1.000E-02	1.06E-01	A				
-9.000E-03	1.11E-01	A				
-8.000E-03	1.15E-01	A				
-7.000E-03	1.20E-01	A				
-6.000E-03	1.25E-01	A				
-5.000E-03	1.31E-01	A				
-4.000E-03	1.35E-01	A				
-3.000E-03	1.43E-01	A				
-2.000E-03	1.51E-01	A				
-1.000E-03	1.60E-01	A				
0.	1.73E-01	A				
1.000E-03	1.93E-01	A				
2.000E-03	5.86E-01	A				
3.000E-03	1.77E+00	A				
4.000E-03	1.79E+00	A				
5.000E-03	1.80E+00	A				
6.000E-03	1.81E+00	A				
7.000E-03	1.82E+00	A				
8.000E-03	1.82E+00	A				
9.000E-03	1.83E+00	A				
1.000E-02	1.83E+00	A				

******* OPERATING POINT INFORMATION TNOH= 27.000 TEMP= 27.000**

NODE	=VOLTAGE	NODE	=VOLTAGE	NODE	=VOLTAGE
+0:1	= 2.000E-03	0:2	= -5.950E-01	0:3	= 1.081E-01
+0:4	= 1.100E-01	0:5	= 1.260E+00	0:6	= 5.857E-01
+0:7	= 1.880E+00	0:8	= 1.879E+00	0:9	= 7.050E-01
+0:10	= 0.	0:100	= 2.500E+00	0:200	= -2.500E+00

****** BIPOLAR JUNCTION TRANSISTORS**

```
SUBCKT
ELEMENT 0:Q1 0:Q2 0:Q3 0:Q4
MODEL 0:NPN 0:NPN 0:NPN 0:NPN
IB 2.644E-07 2.447E-07 2.621E-07 2.439E-07
IC 5.292E-05 4.899E-05 5.265E-05 4.874E-05
VBE 5.970E-01 5.950E-01 5.968E-01 5.950E-01
VCE 7.032E-01 7.050E-01 1.152E+00 4.757E-01
VBC -1.061E-01 -1.100E-01 -5.558E-01 1.192E-01
VS -1.081E-01 -1.100E-01 -1.260E+00 -5.857E-01
POWER 3.737E-05 3.468E-05 6.084E-05 2.333E-05
BETAD 2.001E+02 2.001E+02 2.008E+02 1.998E+02
GM 2.045E-03 1.894E-03 2.035E-03 1.884E-03
RPI 9.783E+04 1.056E+05 9.866E+04 1.060E+05
RX 2.000E+02 2.000E+02 2.000E+02 2.000E+02
RO 2.458E+06 2.656E+06 2.479E+06 2.664E+06
BETAAC 2.001E+02 2.001E+02 2.008E+02 1.997E+02
```

```
SUBCKT
ELEMENT 0:Q5 0:Q6 0:Q7 0:Q8
MODEL 0:PNP 0:PNP 0:PNP 0:PNP
IB -1.014E-06 -9.619E-07 -9.941E-07 -9.941E-07
IC -5.068E-05 -4.874E-05 -4.970E-05 -4.970E-05
VBE -6.199E-01 -6.185E-01 -6.194E-01 -6.194E-01
VCE -6.199E-01 -1.293E+00 -6.194E-01 -6.208E-01
VBC 0. 6.750E-01 0. 1.369E-03
VS -1.261E+00 -1.261E+00 -1.880E+00 -1.880E+00
POWER 3.204E-05 6.364E-05 3.140E-05 3.147E-05
BETAD 5.000E+01 5.067E+01 5.000E+01 5.000E+01
GM 1.958E-03 1.884E-03 1.921E-03 1.921E-03
RPI 2.551E+04 2.689E+04 2.601E+04 2.601E+04
RX 3.000E+02 3.000E+02 3.000E+02 3.000E+02
RO 9.866E+05 1.039E+06 1.006E+06 1.006E+06
BETAAC 4.997E+01 5.064E+01 4.997E+01 4.997E+01
```

****** SMALL-SIGNAL TRANSFER CHARACTERISTICS**

```
V(6)/VI = 4.909E+04
INPUT RESISTANCE AT VI = 2.148E+05
OUTPUT RESISTANCE AT V(6) = 2.611E+07
```

4.22

Circuit as shown in fig (4.31a)

with $V_{CC} = 15V$, $R_1 = 20k\Omega$, $R_2 = 10k\Omega$

$$I_{IN} = \frac{15 - 0.7}{20k\Omega} = 0.72 \text{ mA}$$

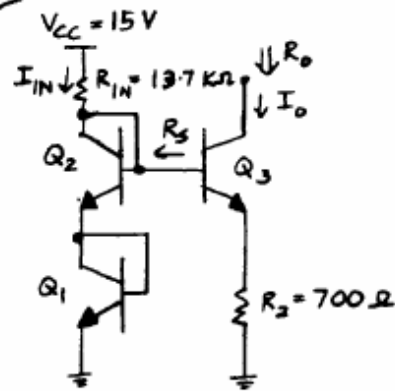
$$I_{OUT} R_2 = V_T \ln \frac{I_{E1}}{I_{OUT}} \approx V_T \ln \frac{I_{IN}}{I_{OUT}}$$

$$I_{OUT} = \frac{V_T}{R_2} \ln \frac{I_{IN}}{I_{OUT}} = 2.6 \times 10^{-6} \ln \frac{0.72 \text{ mA}}{I_{OUT}}$$

By trial and error we find out,

$$I_{OUT} \approx 10.9 \mu\text{A}$$

4.25



Assume :

$$I_S = 5 \times 10^{-15} \text{ A}$$

$$\beta_o = 200$$

$$V_{BE_1} + V_{BE_2} = V_{BE_3} + I_O R_2$$

$$I_{C_1} \approx I_{C_2} = I_{IN} ; I_O = I_{E_3}$$

$$I_{IN} = \frac{15 - 2 \times 0.7}{13.7 \text{ k}} = 0.993 \text{ mA}$$

$$V_T \ln \frac{I_{C_1}}{I_S} + V_T \ln \frac{I_{C_2}}{I_S}$$

$$= V_T \ln \frac{I_O}{I_S} + I_O R_2$$

$$\therefore I_O = \frac{V_T}{R_2} \ln \frac{I_{IN}^2}{I_O I_S} = \frac{26 \text{ mV}}{700 \Omega} \ln \frac{(0.993 \times 10^{-3})^2}{(5 \times 10^{-15} I_O)}$$

By trial and error, $I_O = 0.97 \text{ mA}$ R_S is the equivalent resistancelooking into the base of Q_2

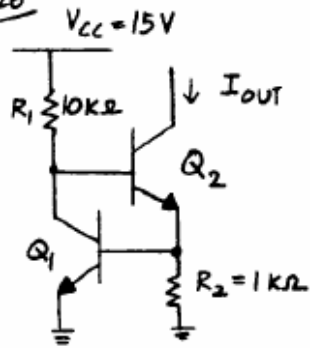
$$R_S \approx \frac{2}{g_m} = 2 \frac{V_T}{I_{IN}} = 52 \Omega \ll r_{\pi_3}$$

where $r_{\pi_3} \approx 2.6 \text{ k}\Omega$ $\therefore g_{m_3} = \frac{1}{26} \text{ V}$

$$R_O = r_{o_3} \left(1 + \frac{g_{m_3} R_2}{1 + g_{m_3} R_2} \right) = 3.2 \text{ M}\Omega$$

where, $r_{o_3} = \frac{V_A}{I_O} \approx 130 \text{ k}\Omega$

4.26



$$S = \frac{V_{CC}}{I_{OUT}} \frac{\partial I_{OUT}}{\partial V_{CC}}$$

For this circuit

$$I_{OUT} \approx \frac{V_{BE1}}{R_2}$$

$$I_{C1} = \frac{V_{CC} - V_{BE1} - V_{BE2}}{R_1} \text{ and}$$

$$V_{BE1} = V_T \ln \frac{I_{C1}}{I_S}$$

$$\therefore I_{OUT} = \frac{V_T}{R_2} \ln \frac{V_{CC} - V_{BE1} - V_{BE2}}{I_S R_1}$$

If $V_{BE(on)} \ll V_{CC}$ then,

$$\frac{\partial I_{OUT}}{\partial V_{CC}} \approx \frac{V_T}{R_2} \frac{1}{V_{CC} - V_{BE1} - V_{BE2}}$$

$$\text{and } S = \frac{V_{CC}}{I_{OUT}} \frac{V_T}{R_2} \frac{1}{V_{CC} - V_{BE1} - V_{BE2}}$$

$$I_{C1} \approx \frac{15 - 0.7 - 0.7}{10} = 1.36 \text{ mA}$$

$$\therefore V_{BE1} \approx 26 \ln \frac{1.36 \times 10^{-3}}{5 \times 10^{-5}} \text{ mV}$$

$$= 0.685 \text{ V}$$

$$\therefore I_{OUT} = \frac{0.685}{1} = 0.685 \text{ mA}$$

$$\therefore S = \frac{15}{0.685 \times 10^{-3}} \frac{26 \times 10^{-3}}{1000} \frac{1}{13.6} = 0.04$$